Laser-Induced Carbon Pyrolysis of Electrodes for Neural Interface Systems

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Abstract—The objective of this work is to produce a laser-fabricated polymer-metal-polymer electrode with the merit of a carbon-based coating as the active site. A 10 µm-thick layer of parylene-C is used serving as the insulating layer in which the active site is locally laser-pyrolyzed. Our preliminary results show that the proposed method is promising in terms of fabrication feasibility and desired electrochemical capabilities.

I. INTRODUCTION

Neural interfacing systems (NIS) can act as a bridge between the body and the exterior world when the communication between the brain and the muscles or organs is compromised [1]. Electrodes are known as one of the most crucial parts of the NIS due to their functionality as an active interface in direct contact with the tissue. Noble metals have been widely used as electrode material for both stimulation and recording applications [2]. However, degradation mechanisms, for example due to limited charge injection capacity restrict their usage [4][5]. Miniaturized interfaces, on which the geometrical surface area for a contact is restricted, challenge the development of new materials with a high electrochemical performance.

Lately, carbon based materials have emerged as a versatile and potential substitutes for metal electrodes [6]. This is attributed to their superior properties such as biocompatibility, chemical inertness, mechanical robustness and good electrochemical properties due to a large effective surface area of contact [4][5][7].

Amongst carbon materials, glassy carbon and Q-carbon appears as very promising materials [8][9]. Glassy carbon has already showed it’s applications in neural prosthetics, with unique electrochemical performance [3][8]. The just recently discovered Q-carbon appeared to be a very promising material by facilitating improved properties such as mechanical hardness, electrical conductivity, chemical and physical characteristics [9].

Q-carbon is produced using a laser and having an amorphous carbon coating as the initial substrate [9]. Glassy carbon for instance can be produced by the pyrolysis of high-carbon content polymers such as Kapton [10] and Su-8 [3]. The typical pyrolysis process consists in using a furnace at high temperatures in an inert atmosphere [7]. This high temperature restricts the fabrication procedure, as it has to take place at the beginning of the microfabrication procedure, unless the electrodes are composed of purely semiconductor or ceramic materials. Photolithography technique can be also employed [7] but it requires the use of masks and clean room facilities which raises the complexity and fabrication costs. However, using the laser as pyrolysis method has also been reported [7][10]. The pyrolysis method using laser is advantageous as compared to the other mentioned methods as it avoids the use of high temperatures and requires no need for the cleanroom processes. Laser technology enables local carbonization at the desired spot, is fast and allows highest flexibility [11].

Within this work, we report on a novel electrode fabrication process that merges the cost, time and production advantages of multiple technological processes to fabricate electrodes with advanced electrochemical performance. The goal of this work is also to investigate the properties of laser-based carbon pyrolysis for electrodes in NIS and bring its development closer to in vivo applications.

The proposed method uses laser-machining to produce structured polymer-metal-polymer electrode arrays. The elegance of the process lies in the fact that the same material serving as a coating and insulation between metal lines is locally transformed by laser to an improved carbon-based coatings at the active sites. The material used as precursor of the carbon-based material is parylene-C which is known as a biocompatible, mechanically robust and medically approved material [2].

II. MATERIALS AND METHODS

A. Process

The fabrication process starts with lamination of self-adhesive tape (No. 4124 by Tesa AG, Hamburg, Germany) onto a ceramic carrier (Fig.1.a). This sheet acts as release layer to separate the electrode from the ceramic carrier in the last step. Then, a layer of approximately 200 µm diluted silicone rubber (MED-1000,NuSil, Carpinteria, USA) was spin coated on top (Fig.1.b). The diluted silicone rubber (with n-heptane in a volume ratio of 1:1) was used in order to yield a more homogeneous coating.

Before the spin coated silicone rubber is fully cured, a thin platinum-iridium foil (25 µm) was laminated onto it (Fig.1.c). A nanosecond pulsed laser (DPL Genesis Marker Nd:YAG, ACI Laser GmbH, Deutschland) was used to cut out the electrode sides, tracks and contacts (Fig.1.d). In order to anchor the foil and the polymers, additional small openings were introduced in the outer vicinity of the electrode active site [2].

Having removed the excess metal with tweezers, a parylene-C (DPXC by Specialty Coating Systems, Indianapolis, USA) layer of 10 µm is deposited on top (Fig.1.e-f) with a parylene-C deposition unit (PDS 2010 LAB-COTERTM by Specialty Coating Systems, Indianapolis, USA). This polymer has a high quantity of carbon in composition which makes it suitable to be a precursor of the carbonized material.

Using the same laser, but different parameters, the parylene-C was carbonized by pyrolysis at the desired site on top of the platinum layer. Here, the pyrolyzed material forms a conductive connection to the platinum-iridium foil (Fig.1.g). Laser ablation was used, to remove the Parylene-C at the distal end from the interconnection contact pad and also to cut the perimeter of the array. Reference electrodes with no carbon coating were produced by cutting the perimeter of the

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electrode site and peeling off excess material from the surface. Lastly, the electrode was peeled off the release layer. (Fig. 1.h-i).

The used laser was an infrared nanosecond (pulse width of 30 to 90 ns) with wavelength of 1064 nm. Therefore the interaction with the materials was predominantly of thermal nature [12]. In order to avoid burning of the material, all experiments were performed in saturated N₂ environment. The usage of laser causes the material to reach a certain temperature in which volatile elements are removed, new C-C bonds are formed and hence, the polymer pyrolysis can be realized [6]. Since the plasma temperature at the laser focus point (35 µm in diameter) is influenced by the material characteristics, laser parameters and environmental conditions [13], a scope of laser parameters to generate carbon electrodes was studied. The laser parameters have especially high influence on the power density reaching the sample and therefore in the generation of the desired material [9].

The best combination of laser parameters i.e. power, frequency, speed and pulse duration, was used to produce an electrode active site of 700 µm in diameter. All materials used to fabricate the samples were biocompatible and medical grade.

Figure 1. Cross-section schematic of the array process fabrication: a. lamination of the release layer; b. spin coat PDMS; c. lamination of the metal; d. laser structuring of the metal; e. removal of metal excess; f. parylene-C deposition; g. laser pyrolysis; h. contact opening and cut of the electrode borders; i. electrode peel off.

B. Composition of electrodes

Composition analysis of the carbonized electrodes was done using X-ray photoelectron spectroscopy (XPS). The measurements were performed using a K-Alpha+ XPS spectrometer (Thermo Fisher Scientific, East Grinstead, UK). Data acquisition and processing using the Thermo Advantage software is described elsewhere [14]. The sample was analyzed using a microfocused, monochromated Al Kα X-ray source (30-400 µm spot size). The spectra were fitted with one or more Voigt profiles (binding energy uncertainty: ±0.2 eV). The analyzer transmission function, Scofield sensitivity factors [15] and effective attenuation lengths (EALs) for photoelectrons were applied for quantification. EALs were calculated using the standard TPP-2M formalism [16]. All spectra were referenced to the Cls peak of hydrocarbon at 285.0 eV binding energy controlled by means of the well-known photoelectron peaks of metallic Cu, Ag, and Au. Prior to spectral measurements the samples were sputter cleaned using an Ar1000+ cluster ion beam at 8 keV and 30° angle of incidence which did not harm the arrays.

C. Conductance Test

In order to have an estimation of the conductance (σ) of the pyrolyzed material the resistance (ρ) was measure according to (1).

\[ \sigma = \frac{1}{\rho} \]  

(1)

The measurements (n=10) were taken at different positions (a, b and c) versus an origin point (0) using an ohmmeter (34401A 6 1/2 Digit Multimeter, Agilent) with two microneedles (see Fig.2). Special care was taken when placing the needles to ensure minimal scratching of the surface. The distance between the origin point and the a, b and c point was approximately 0.3, 0.6 and 10 mm, respectively. Here a and b were located inside the pyrolyzed area and point c was found at the electrode contact.

Figure 2. Setup used to achieve a conductance approximation. Electrode active site (left) and contact pad (right) are connected via an insulated metal line under the top layer (not shown in the graph).

D. Electrochemical Characterization

Electrochemical characterization of the fabricated electrodes was addressed using electrochemical impedance spectroscopy (EIS) and cyclic voltammetry (CV). Measurements were performed in a three electrode setup with a platinum counter electrode and Ag/AgCl reference electrode. Both CV and EIS were conducted in 0.9% saline solution. Electrochemical interface was provided by a potentiostat and a frequency analyzer device (Solartron 1260&1287 by Solartron Analytical, Fareham, Hampshire, UK) accompanied by the software Zplot (v2.8 by Scribner Associates Inc., Southern Pines, NC, USA) to control the setup, and save and analyze the data. The EIS measurements were made within the frequency range of 0.1 Hz -1 MHz with an excitation amplitude of 0.5 mV. In order to run CV measurements the vertex potentials were set between -0.6 mV and 0.8 mV and the working electrode potential was swept at a scan rate of 50 mV/s.

E. Pulse Test

Pulse test (voltage transient measurement) was used to study the maximum polarization, both most negative (E_{max}) and most positive (E_{max}), of the electrode-electrolyte interface under a current-controlled stimulation pulse. This test was conducted in phosphate buffered saline (PBS). The used current pulse was a rectangular shaped, symmetrical, biphasic, charge balanced, negative phase first waveform. The amplitude was set at 200 µA (pulse width of 200 µs and the pulse repetition frequency of 20 Hz).

III. PRELIMINARY RESULTS

A. Process

In this work samples with simple structure designs were produced as can be seen in (Fig.3.a). Is also notable that the using of polymers provides flexibility, not compromising its robustness. Through optical inspection with microscope (LEICA DM4000M), the surface structure of the pyrolyzed active site shows to be rough (Fig.3.b).
B. Composition of electrodes

One sample was analyzed with XPS to reveal the chemical and elemental composition of the original insulation layer (parylene-C) and the pyrolyzed electrode. The dominating atomic bonds in parylene-C are 78.3% carbon-hydrogen (C-H, Cls=285.0 eV) and 8.7% carbon-oxygen (C-O, Cls=286.8 eV). There are no indicators for graphitic carbon or for the underlying platinum, nor high concentrations of salts. In contrast, the carbonized area consist mainly of graphitic carbon at Cls=284.4 eV (51.5%), some C-H leftovers (13.4%) and a high amount of sodium (13.4%) and chloride (13.0%). Beside other minor contaminations, little platinum (< 2%) is exposed on the electrode surface.

C. Conductance Test

The pyrolyzed material is conductive, presenting a mean conductance at position a and b of about 0.4 S and 0.3 S, respectively (Fig. 5, black markers). Furthermore, a conductive transition between the pyrolyzed layer and the metal layer can be verified from the values measured at position c. The conductivity for Pt:Ir was measured slightly higher (approx. 0.5 S, Fig.5 white markers).

D. Electrochemical Characterization

To study the electrode performance under stress conditions, some electrodes were cycled for a longer time frame, i.e. 90 cycles at scan rate of 200 mV/s. The impedance magnitude of the pyrolyzed electrode was found to be about 55 KΩ higher than the measured impedance for the reference (see Fig.6). The impedance behavior of the pyrolyzed samples remained approximately the same after 70 cycles of the cyclic voltammometric stress (Fig.7) but showed a decrease after 90 cycles.

The obtained cyclic voltammograms revealed an increase in the charge storage capacity (CSC) in the pyrolyzed electrodes after 70 cycles of voltammometric stress (Fig.7). It is also noticed that the voltammogram shape of the pyrolyzed material differs from the reference including a wider water window (Fig.8).

E. Pulse Test

The injected charge density obtained from the used waveform corresponds to 10.3 µC/cm², calculated using (2).

\[ Q = \frac{I \cdot t}{A} \]

(2)

Where Q (µC/cm²) is the charge density, I is the applied current (A), t is the pulse width (µs) and A (cm²) is the geometric surface area of the electrode.

The measured potential drop across the access resistance was found to be roughly the same for both the pyrolyzed electrode and the Pt:Ir reference, corresponding to approximately 100 mV (Fig.9, initial step).

The pulse test, as described in method section resulted in Eacc of, approximately 1 V in case of pyrolyzed electrodes which was about 700 mV higher than the measured value for the reference Pt-Ir (Fig.9). However, after stressing the electrode by cyclic voltammetry the Eacc experienced a drop of, approximately, 300 mV.

The voltage excursion observed for the pyrolyzed material remained within the water window limit throughout the measurement even in case of ramping up the injected current up to 1000 µA.
conditions have been detected, the presented method remains an accessible way to further study the local pyrolysis of carbon into a desired composition for the target application. The proof of concept was provided. However, more investigation is yet needed in order to obtain a better understanding of the surface characteristics and also to address the biocompatibility and biostability concerns.

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